

Numerical study of quantum turbulence in superfluid helium

HVBK two-fluid model

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ANR Project QUTE-HPC (2019-2023)

10 members = 5 Physics + 5 Mathematics

- (HPC) parallel codes for QT :: open source,
- huge simulations of physical configurations (compare with our own experiments).

<http://qute-hpc.math.cnrs.fr/>

1 Two-fluid HVBK model and quantum turbulence

- Two-fluid conception of superfluid helium
- Quantum turbulence and vortex lines
- The HVBK model and the mutual friction force

2 Results of direct simulation of HVBK

- Hydrodynamic behaviors accounting for the mutual friction
- The role of the friction force on the energy budget
- The role of the friction force on the turbulence intermittency

Liquide Helium under 2.1K viscous paradox: frictionless but viscous

@Alfred Leitner 1963 from Michigan stat university

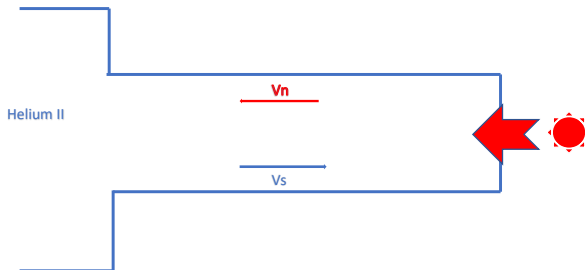
- The superfluid:
 - no viscosity
 - free of entropy
- The normal fluid:
 - viscosity
 - carries entropy

helium II two-fluids model (Landau 1941)

- Normal fluid: ρ_n, v_n, ν_n
- Superfluid: ρ_s, v_s
- For $0K < T < T_\lambda$ mixture of two fluid $\rho = \rho_n + \rho_s$, for $T > T_\lambda$, $\rho_s/\rho = 0$; for $T = 0K$, $\rho_n/\rho = 0$

Thermal counter-flow and quantum turbulence

Second sound wave oscillation of T and S, first sound wave oscillation of ρ and P



$$Q = \rho S T v_n, \quad j = \rho_s v_s + \rho_n v_n = 0 \quad \text{and} \quad V_{ns} = v_n - v_s = Q / (S T \rho_s)$$

Heat transfer in liquid helium like a sound wave

$$\text{"Second sound"} \quad u_2^2 = T S^2 \rho_s / C \rho_n$$

$Q > Q_{critical}$ then vortex lines are created

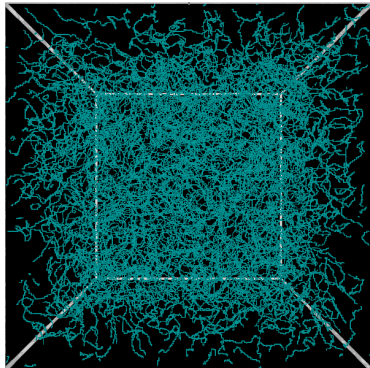
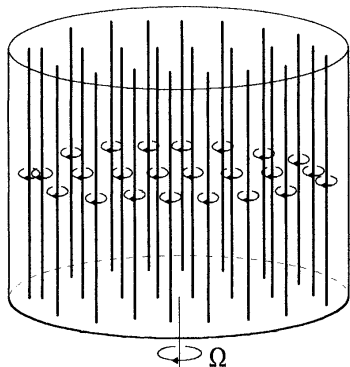
Quantum turbulence contains a large number of randomly distributed vortex lines

Vortex lines in helium II

- The circulation is quantized in unit circulation of $\frac{\hbar}{m}$, with \hbar is the Plank's constant and m is the helium atom mass, thus

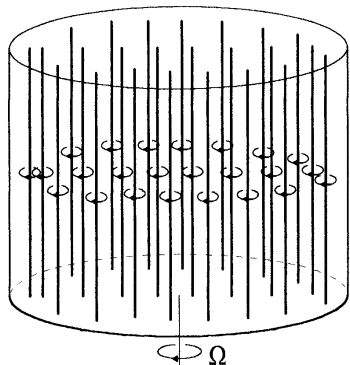
$$\kappa = \oint \mathbf{v}_s \cdot d\mathbf{r} = \frac{\hbar}{m}, \quad \omega = 2\Omega = n\kappa$$

with ω is the voricity of rotating solide body and n is the volume line density



Vortex lines and mutual friction force

The experiment of second sound wave attenuation propagating in rotating helium II [Vinen & Hall 1956].



$$\frac{A}{A_0} = \left(1 + \frac{2\Omega}{76.1}\right)^{-1}$$

Mutual friction force

- A volume force: independent to the geometric nor the position
- depends on the relative orientation of relative velocity and the rotating axis
- depends on the angular velocity Ω .
Feynman's rule: $2\Omega = \nabla \times v_s = \kappa \mathcal{L}$.
- Model: Each vortex line is the scattering center of the excitation (rotons), where brings the momentum exchange (Newton's Laws)

The mutual friction force writes:

$$\mathbf{F}_M = -B \frac{\rho_s \rho_n}{\rho} \frac{\boldsymbol{\omega} \wedge (\boldsymbol{\omega} \wedge (\mathbf{v}_s - \mathbf{v}_n))}{|\boldsymbol{\omega}|} - B' \frac{\rho_s \rho_n}{\rho} \boldsymbol{\omega} \wedge (\mathbf{v}_s - \mathbf{v}_n) \quad (1)$$

with B and B' are two temperature dependent parameter, and $\boldsymbol{\omega} = \nabla \times \mathbf{v}_s$, \mathbf{v}_n is the normal fluid velocity and \mathbf{v}_s is the superfluid velocity.

The governing equations write:

$$\nabla \cdot \mathbf{v}_n = 0, \quad \nabla \cdot \mathbf{v}_s = 0 \quad (2)$$

$$\frac{\partial \mathbf{v}_n}{\partial t} + \nabla \cdot (\mathbf{v}_n \otimes \mathbf{v}_n) = -\nabla p_n + \frac{1}{\rho_n} \mathbf{F}_M + \nu_n \Delta \mathbf{v}_n + \mathbf{f}_{ext} \quad (3)$$

$$\frac{\partial \mathbf{v}_s}{\partial t} + \nabla \cdot (\mathbf{v}_s \otimes \mathbf{v}_s) = -\nabla p_s - \frac{1}{\rho_s} \mathbf{F}_M + \nu_s \Delta \mathbf{v}_s + \mathbf{f}_{ext} \quad (4)$$

Vortex lines polarized? turbulence \rightarrow random vortex lines, bundle coherent structure
 Good estimation on macroscopic scales

Code HVBK 3d turbulence: p3dffft(2D decomp), pseudo-spectral method, 3D periodic boundary conditions. Parallel computing on cluster Myria CRIANN.

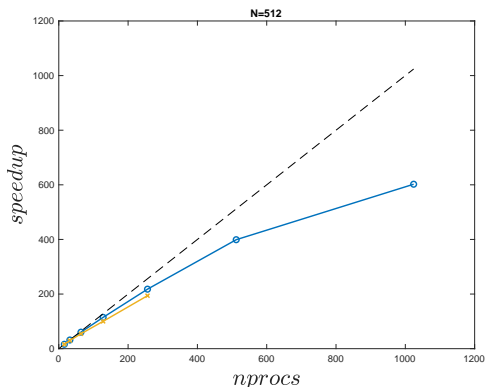


Figure: The scaling test N=512 of code (○) 2D decomposition (x)1D decomposition, Speedup = $\text{Time}(nprocs = 1) / \text{Time}(nprocs = N)$.

Direct simulation of HVBK

- The slope "-5/3" on inertial scales of energy spectrum, dissipation scale decreases with temperature decreases, the coupling energy loss due to the relative velocity.

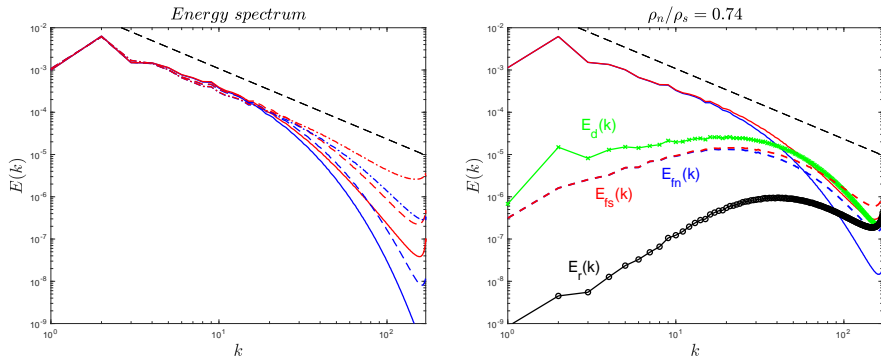


Figure: (a) Turbulence energy spectrum for different temperature (density ratios); (b) Spectrum for dissipation, relative velocity and mutual friction force energy.

- Two fluid are strongly correlated with each other, the energy exchanging is strongly associate to the vorticity.

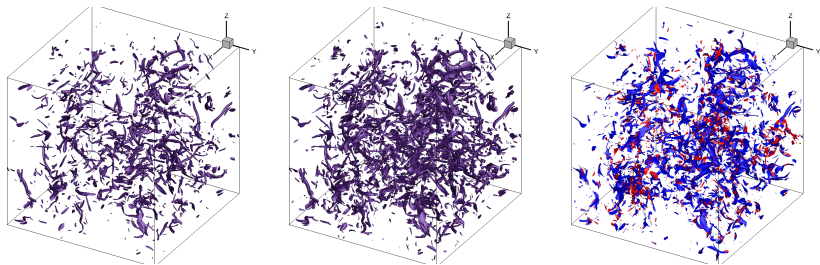


Figure: (a) Snapshot of iso-contour $\omega_n^2 = 5rms(\omega_s^2)$ in normal fluid, (b) Snapshot of $\omega_s^2 = 5rms(\omega_s^2)$ in super fluid, (c) Energy exchange $un.Fns$ in normal fluid. (blue) iso-contour of $6rms$, (red) iso-contour of $-3rms$.

- The energy exchange mainly occurs in the intense vorticity region and it is intermittent.

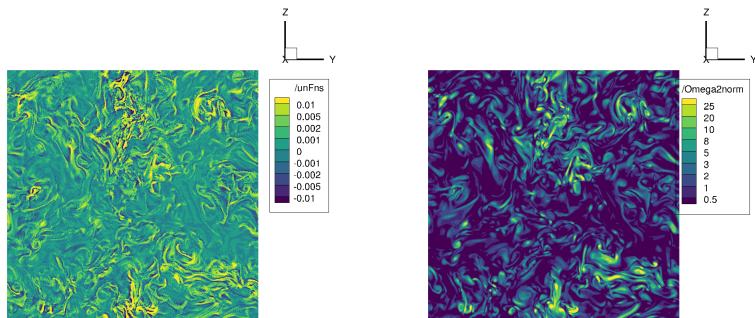


Figure: (left) The energy exchange in normal fluid $u_n \cdot F_{ns}$, (right) the enstrophy of normal fluid $|\Omega_n|^2$

Direct simulation of HVBK

- The dissipation rate ε follows the log-normal PDF according to the eddy-cascade Richardson model as well as the coupling energy PDF.

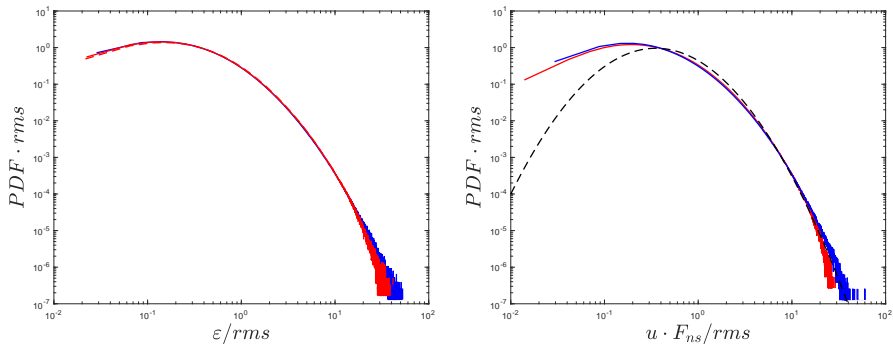


Figure: (left) The normalised P.D.F of locale viscous energy transfers rate, the form is similar to a log-normal distribution (well known as the classical turbulent). (right) The normalised P.D.F of locale energy exchanging rate (red) ϕ_n and (blue) ϕ_s , (- -) a log-normal distribution with $\mu = -\frac{\sigma^2}{2}$ and $\sigma^2 = 0.6931$.

The scales-by-scales energy budget

We follow the classical approach in HIT for the second order structure function transport equations, and integration from 0 to r obtain the 4/3 law, viz.

$$-\overline{\delta u_{\parallel}^n (\delta u_i^n)^2} - \frac{1}{r^2} \int_0^r s^2 \mathcal{L}^n ds + 2\nu_n \frac{d}{dr} \overline{(\delta u_i^n)^2} = \frac{4}{3} \bar{\epsilon}^n r, \quad (5)$$

$$-\overline{\delta u_{\parallel}^s (\delta u_i^s)^2} - \frac{1}{r^2} \int_0^r s^2 \mathcal{L}^s ds + 2\nu_s \frac{d}{dr} \overline{(\delta u_i^s)^2} = \frac{4}{3} \bar{\epsilon}^s r, \quad (6)$$

with

$$\mathcal{L}^n \equiv -2 \frac{\rho_s}{\rho} \overline{(\delta u_i^n) (\delta F_i^{ns})} - 2 \overline{(\delta u_i^n) (\delta f_i^n)}, \quad (7)$$

$$\mathcal{L}^s \equiv 2 \frac{\rho_n}{\rho} \overline{(\delta u_i^s) (\delta F_i^{ns})} - 2 \overline{(\delta u_i^s) (\delta f_i^s)}, \quad (8)$$

where u_{\parallel} is the velocity component parallel to vector \vec{r} , $r = |\vec{r}|$, $\delta f = f(\vec{x} + \vec{r}) - f(\vec{x})$ and for isotropic δf depends only r

The scales-by-scales energy budget

$$-\overline{\delta u_{\parallel}(\delta u_i)^2} - \frac{1}{r^2} \int_0^r s^2 \mathcal{L} ds + 2\nu \frac{d}{dr} \overline{(\delta u_i)^2} = \frac{4}{3} \bar{\epsilon} r, \quad (9)$$

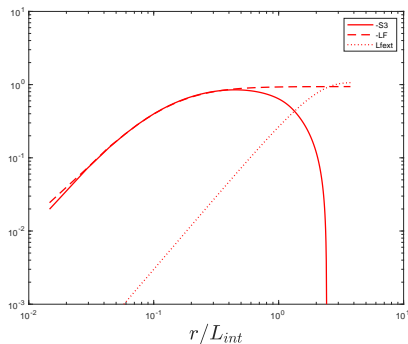
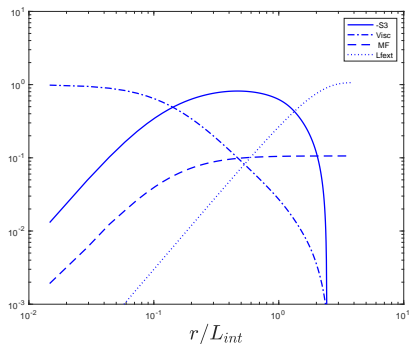


Figure: The case $\rho_n/\rho = 0.9$ and $\nu_s = 0$ (—) The convection term $-\overline{\delta u_{\parallel}(\delta u_i)^2}$, (- -) the mutual friction term $2 \frac{\rho_s}{\rho} \frac{1}{r^2} \int_0^r s^2 \overline{(\delta u_i^n)(\delta F_i^{ns})} ds$ for normal fluid and $2 \frac{\rho_n}{\rho} \frac{1}{r^2} \int_0^r s^2 \overline{(\delta u_i^s)(\delta F_i^{ns})} ds$ (— •) the viscous term (•••) the external forcing term. Normalised by $4/3\bar{\epsilon}^n$

The scales-by-scales energy budget

$$-\overline{\delta u_{\parallel}(\delta u_i)^2} - \frac{1}{r^2} \int_0^r s^2 \mathcal{L} ds + 2\nu \frac{d}{dr} \overline{(\delta u_i)^2} = \frac{4}{3} \bar{\epsilon} r, \quad (10)$$

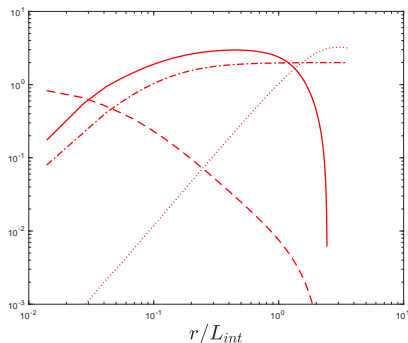
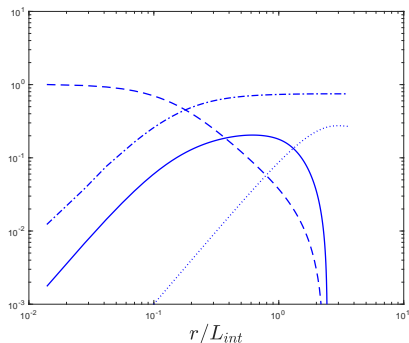


Figure: The case $\rho_n/\rho = 0.1$ and $\nu_s = 0.1\nu_n$ (—) The convection term $-\overline{\delta u_{\parallel}(\delta u_i)^2}$, (- -) the mutual friction term $2 \frac{\rho_s}{\rho} \frac{1}{r^2} \int_0^r s^2 \overline{(\delta u_i^n)(\delta F_i^{ns})} ds$ for normal fluid and $2 \frac{\rho_n}{\rho} \frac{1}{r^2} \int_0^r s^2 \overline{(\delta u_i^s)(\delta F_i^{ns})} ds$ (- •) the viscous term (•••) the external forcing term. Normalised by $4/3\epsilon^n$ for the normal fluid and Normalised by $4/3\epsilon^s$ for the superfluid.

The vortex stretching and the intermittency

$$\partial_t D_{111} + \left(\partial_r + \frac{2}{r} \right) D_{1111} - \frac{6}{r} D_{1122} = -T_{111} + 2\nu C - 2\nu Z_{111} + MF + F_{ext}, \quad (11)$$

with $\partial_r \equiv \partial/\partial r$,

$$\begin{aligned} D_{111} &= \overline{(\delta u)^3}; \\ D_{1111} &= \overline{(\delta u)^4}; \\ D_{1122} &= \overline{(\delta u)^2(\delta v)^2}; \\ C(r, t) &= -\frac{4}{r^2} D_{1111}(r, t) + \frac{4}{r} \partial_r D_{1111} + \partial_r \partial_r D_{1111}; \\ Z_{111} &= \overline{3\delta u \left[\left(\frac{\partial u}{\partial x_l} \right)^2 + \left(\frac{\partial u'}{\partial x'_l} \right)^2 \right]}, \end{aligned} \quad (12)$$

where $\delta u = u(x+r) - u(x)$ is the longitudinal velocity increment, $\delta v = v(x+r) - v(x)$ is the transverse velocity increment and double indices indicate summation and a prime denotes variables at point $x+r$. Finally,

$$T_{111} = \overline{3(\delta u)^2 \delta \left(\frac{\partial p}{\partial x} \right)}. \quad (13)$$

The vortex stretching and the intermittency

$$\partial_t D_{1111} + \left(\partial_r + \frac{2}{r} \right) D_{1111} - \frac{6}{r} D_{1122} = -T_{111} + 2\nu C - 2\nu Z_{111} + MF + F_{ext}, \quad (14)$$

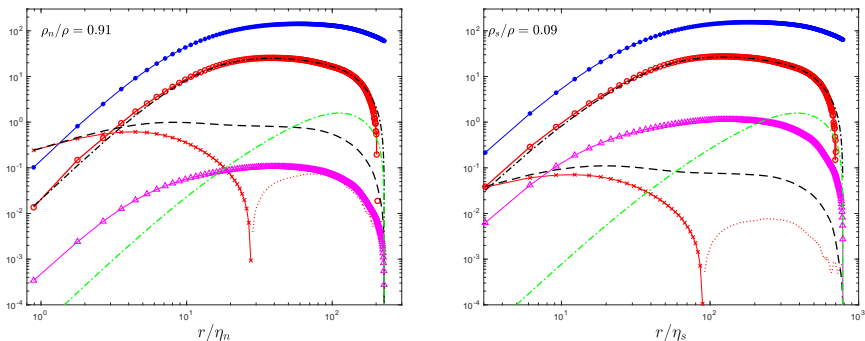


Figure: Balances of different terms in equations for the normal fluid (left) and the superfluid (right) for density ratios $\rho_n/\rho = 0.91$. (●-) $(\partial_r + 2/r)D_{1111}$, (○-) $(\partial_r + 2/r)D_{1111} - 6/r.D_{1122}$, (black -) $-T_{111}$, (×-) $-2\nu C$ (· · ·) positive part of $2\nu C$, (- -) $-2\nu Z_{111}$, (△-) coupling terms, (green -) for the external forcing term. The plots are dimensionless.

The vortex stretching and the intermittency

$$\partial_t D_{1111} + \left(\partial_r + \frac{2}{r} \right) D_{1111} - \frac{6}{r} D_{1122} = -T_{111} + 2\nu C - 2\nu Z_{111} + MF + F_{ext}, \quad (15)$$

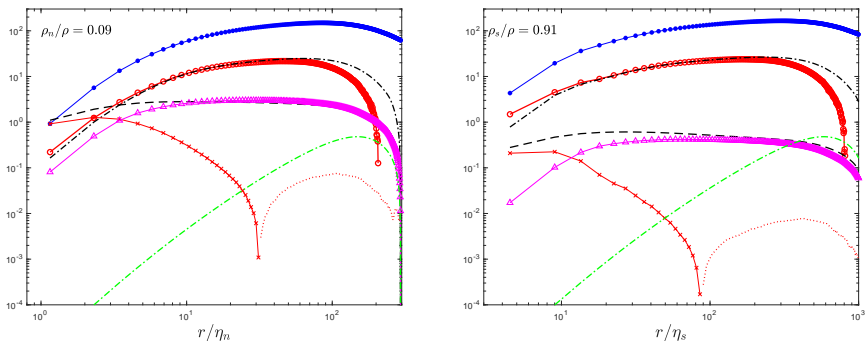


Figure: Balances of different terms in equations for the normal fluid (left) and the superfluid (right) for density ratios $\rho_n/\rho = 0.09$. (●-) $(\partial_r + 2/r)D_{1111}$, (○-) $(\partial_r + 2/r)D_{1111} - 6/r \cdot D_{1122}$, (black - -) $-T_{111}$, (×-) $-2\nu C$ (· · ·) positive part of $2\nu C$, (- -) $-2\nu Z_{111}$, (△-) coupling terms, (green - -) for the external forcing term. The plots are dimensionless.

HVBK two-fluid model DNS show that:

- The normal fluid and the superfluid are highly correlated due to the mutual friction in large scales.
- The mutual friction exchange momentum between the two fluid component, averagely it extract energy from the superfluid and add energy to the normal fluid.
- The large energy exchange mainly happens at the strong vorticity region, which is an intermittent effect.
- The mutual friction has a very important impact to the energy balance. The energy cascading in the inertial sub-range are characterised by both the local dissipation rate and the mutual friction energy exchanging.
- The mutual friction has little impact on the vortex stretching, thus having limited influence to the intermittency of the turbulence.

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